

***Theory of two-step electrode transformations
coupled with chemical equilibria relevant to
electrochemistry of lipophilic redox enzymes
studied under conditions of square-wave
voltammetry***

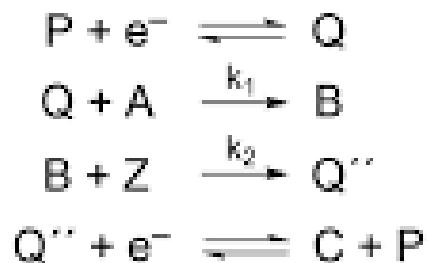
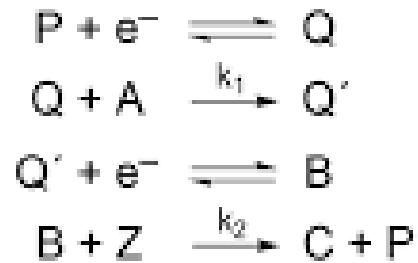
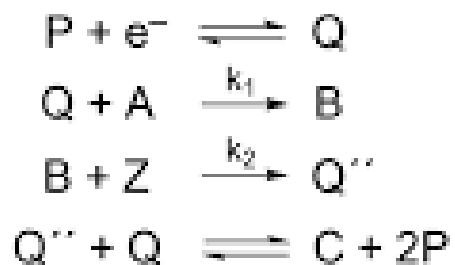
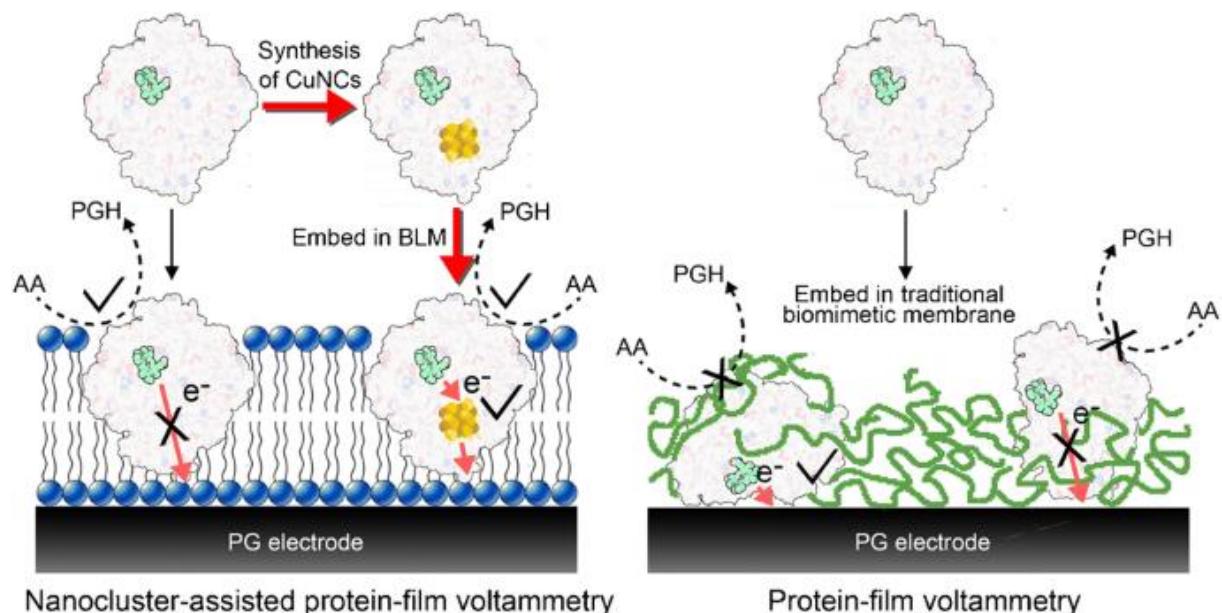
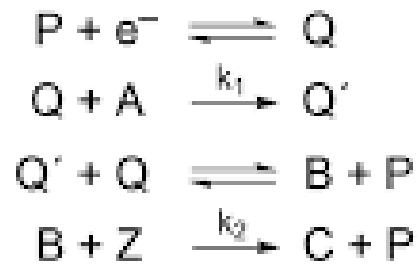
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Abstract

Protein-film voltammetry is recognized as a simple but useful technique that can provide access to the electrochemical features of various lipophilic redox enzymes. The so-called “two-step electrode mechanisms” pare related to the redox chemistry of relevant enzymatic systems whose redox transformation occurs in two consecutive steps. In our recent works we published several theories of two-step electrode mechanisms, in which the electron transfer steps were associated with preceding, follow up or regenerative chemical step. In this work, we present some of the major achievements of the protein-film voltammetry of two-step electrode mechanisms coupled with various chemical equilibria. We also provide the readers several hints on how to use methodologies for the determination of thermodynamic and kinetic parameters relevant to two-step protein-film mechanisms. The considered mechanisms are applicable to many lipophilic redox proteins and enzymes that undergo electrochemical transformations in more than one successive electron steps. Such examples exist by proteins containing quinone moiety and some polyvalent ions of transition metals as redox active sites.

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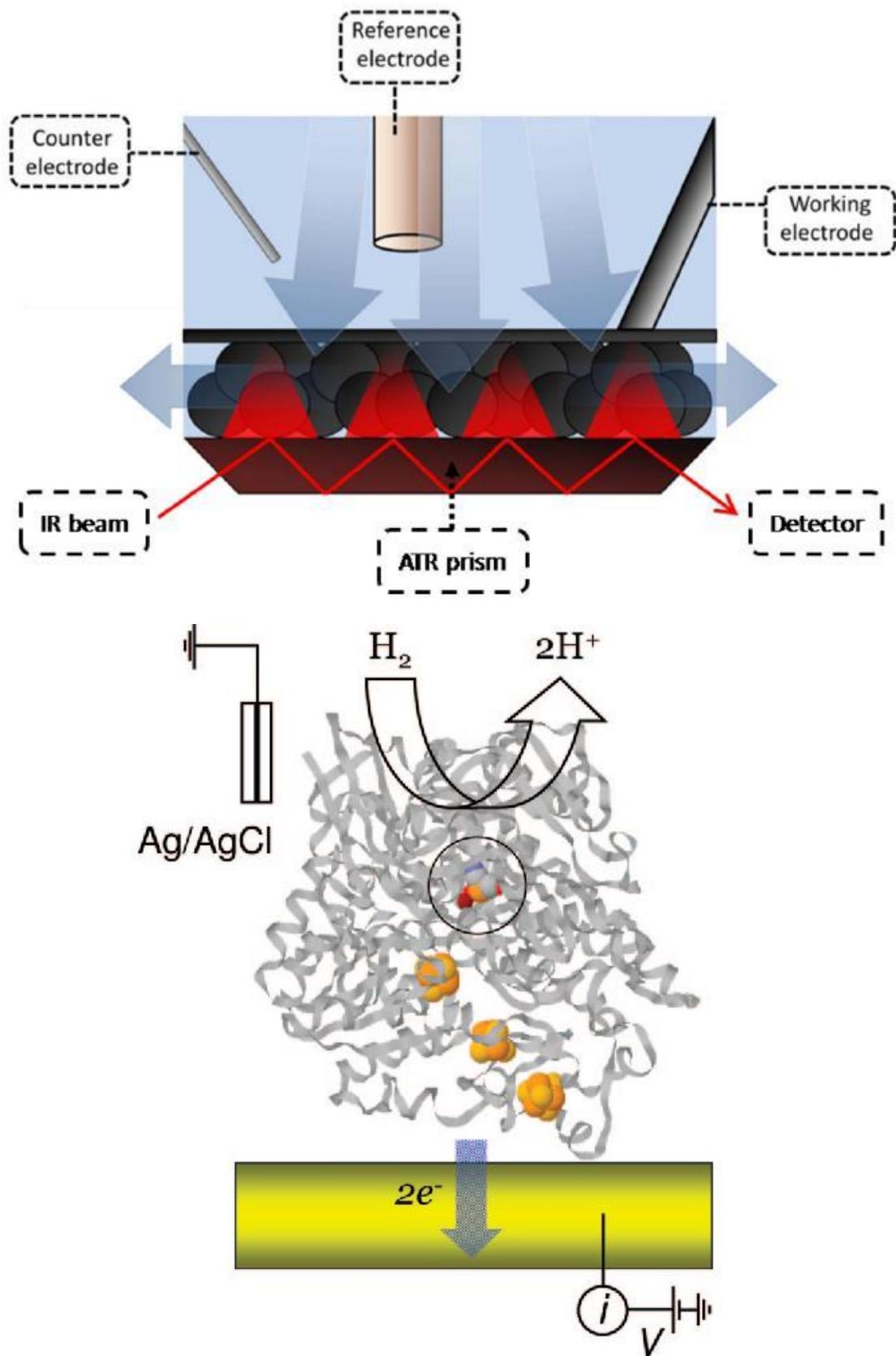
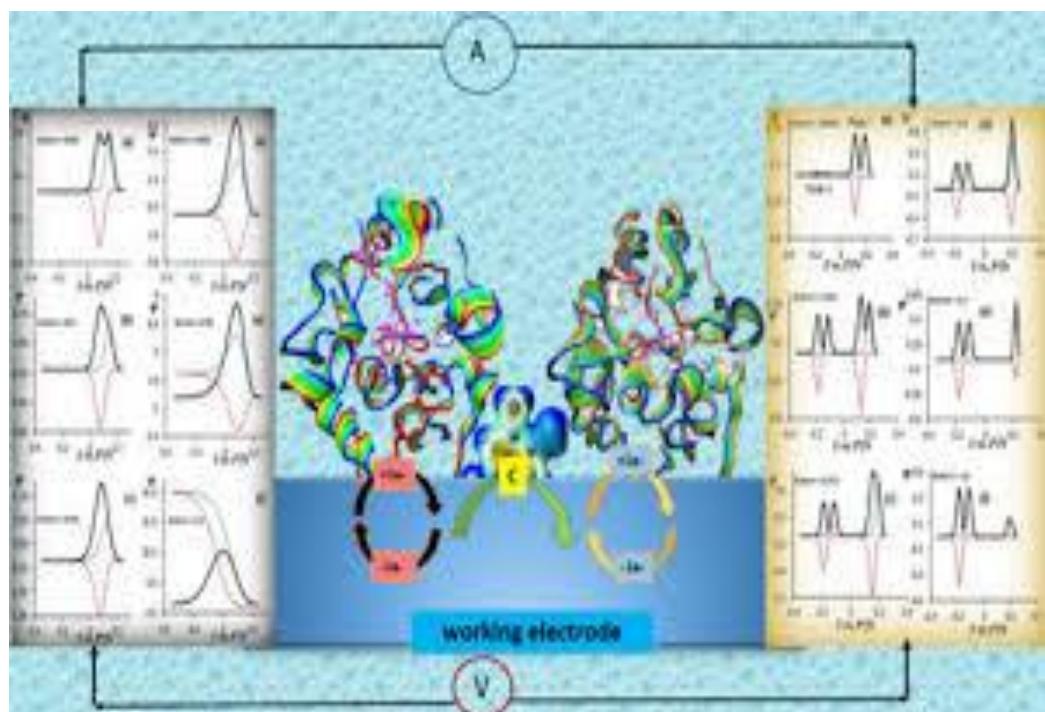
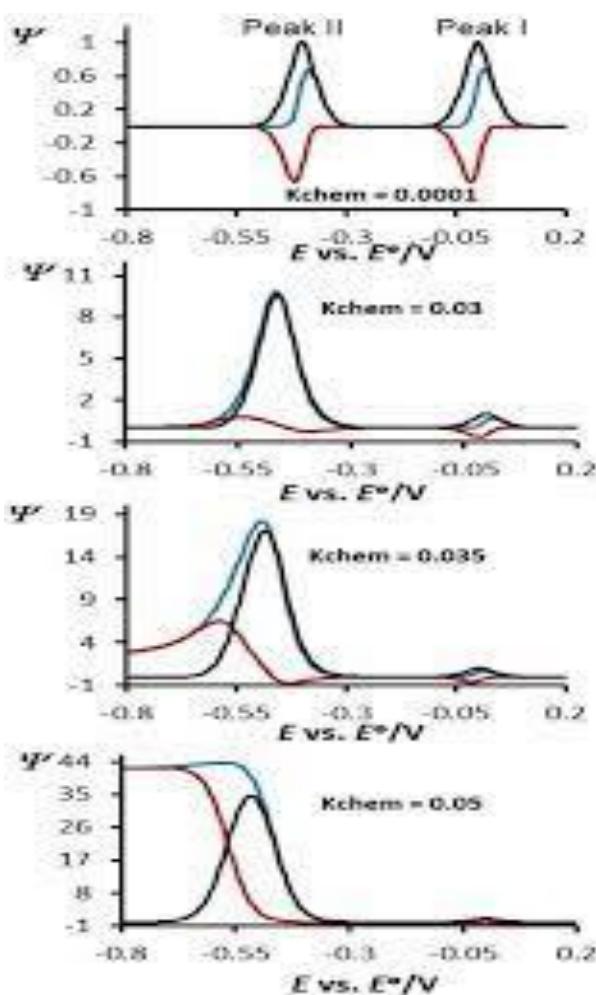
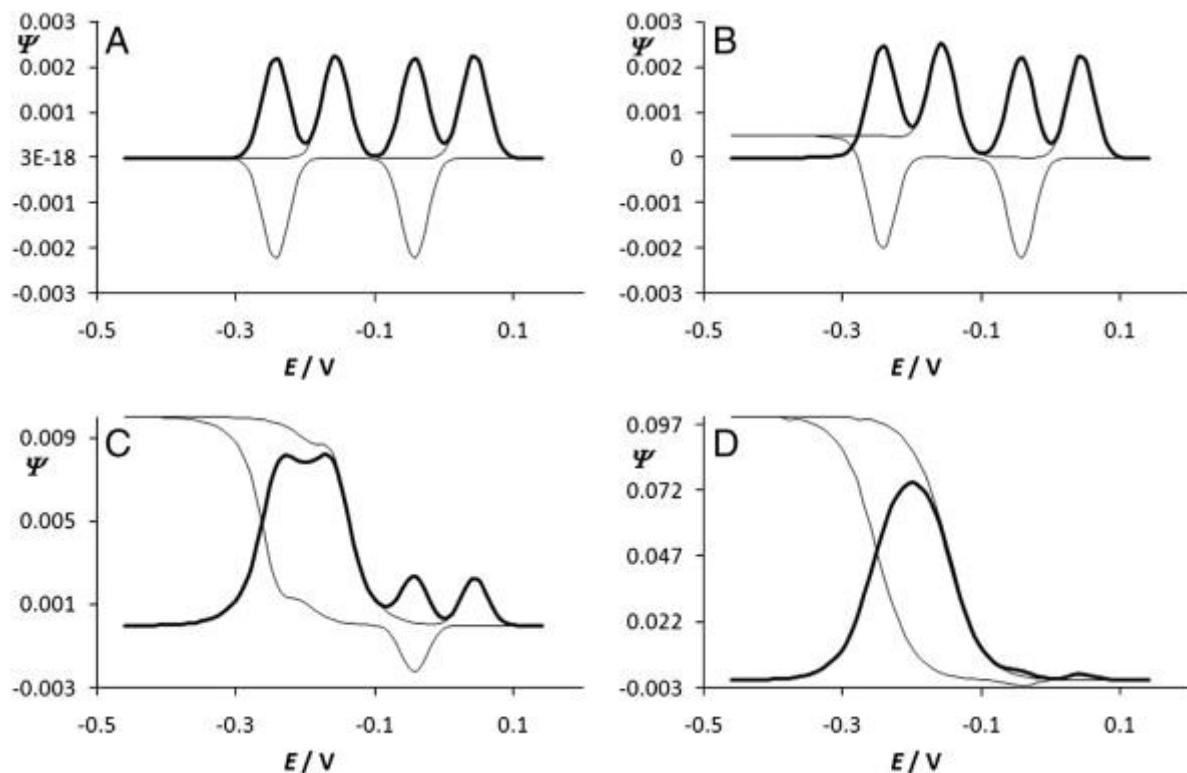
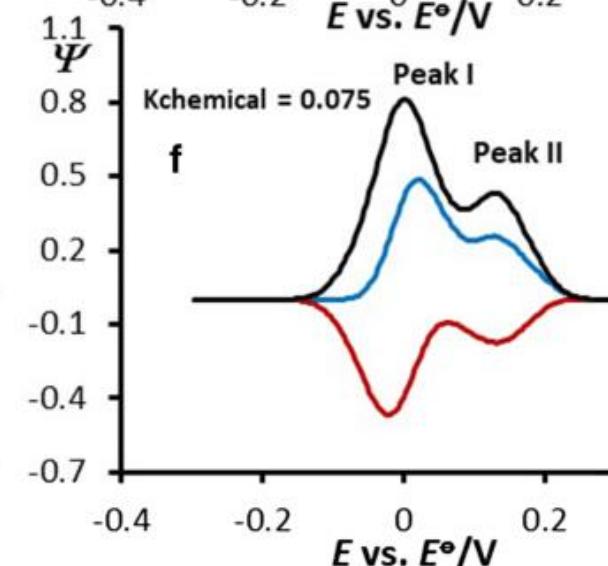
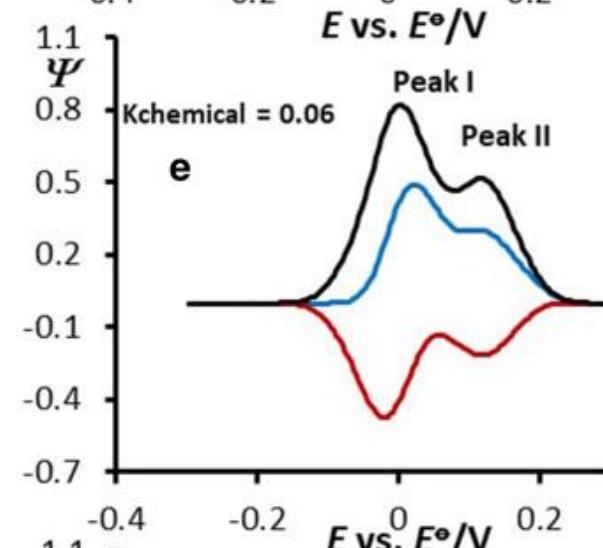
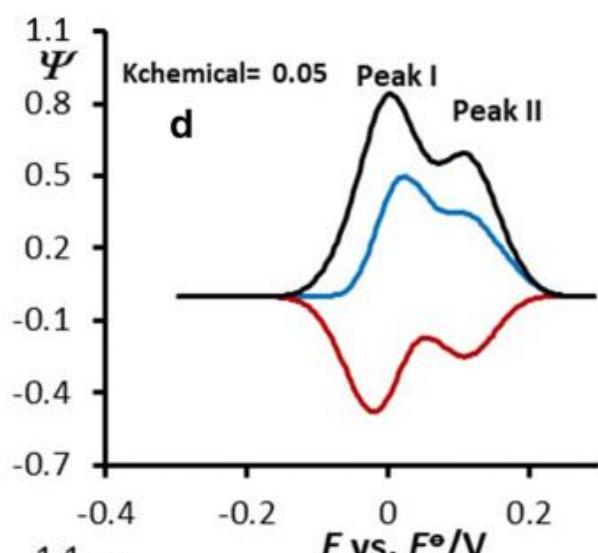
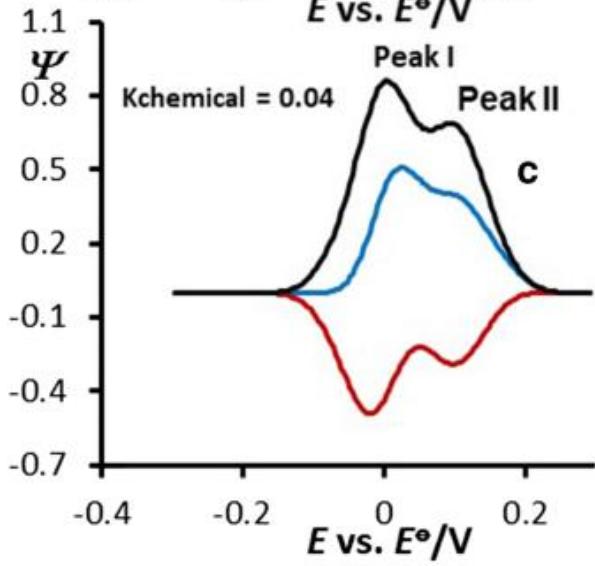
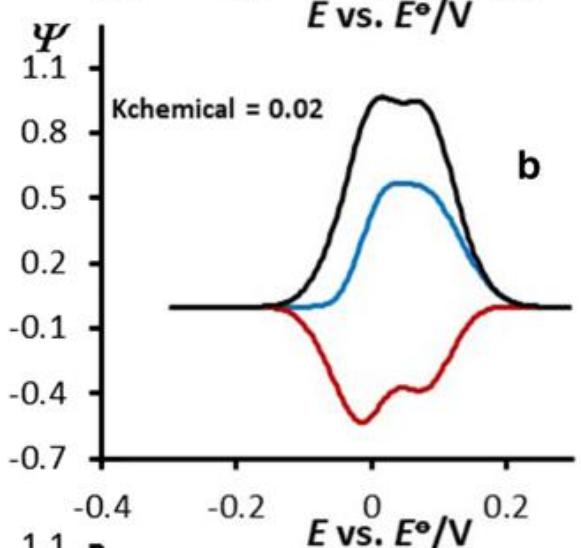
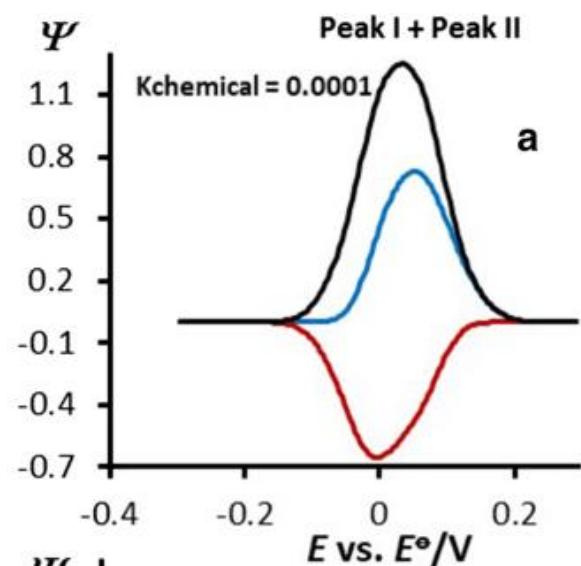
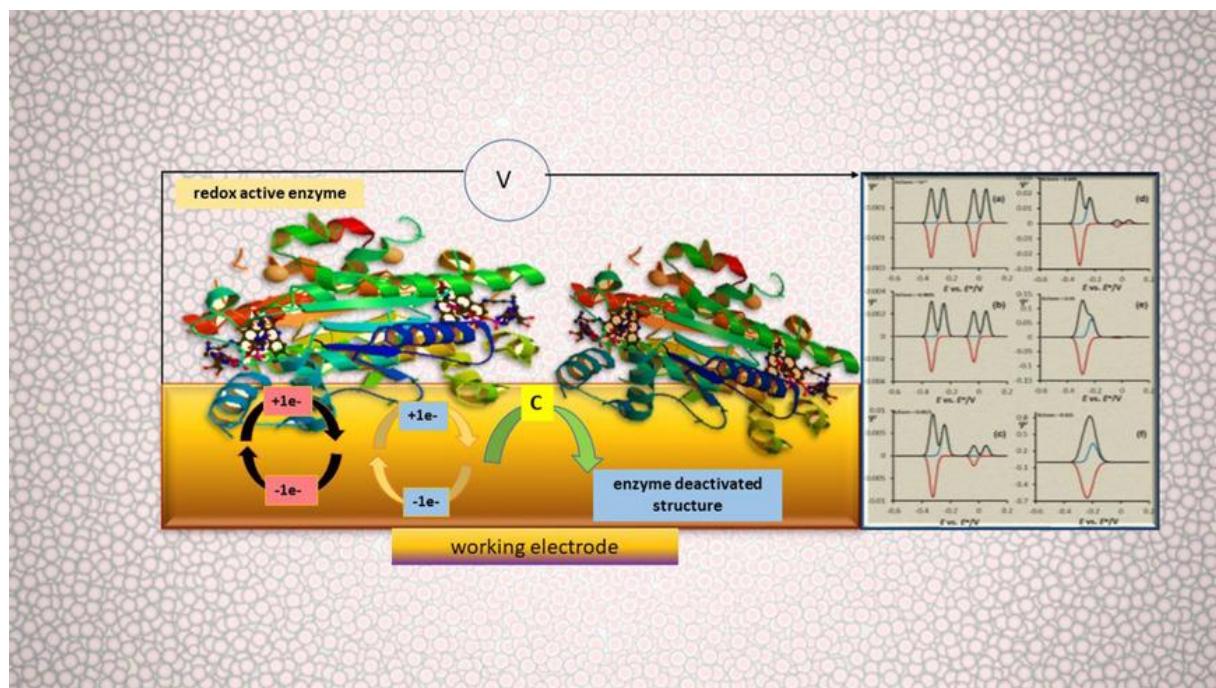
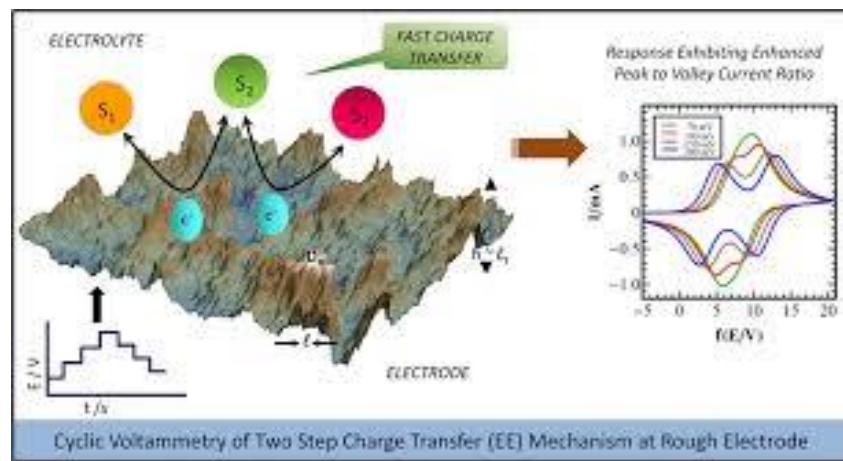


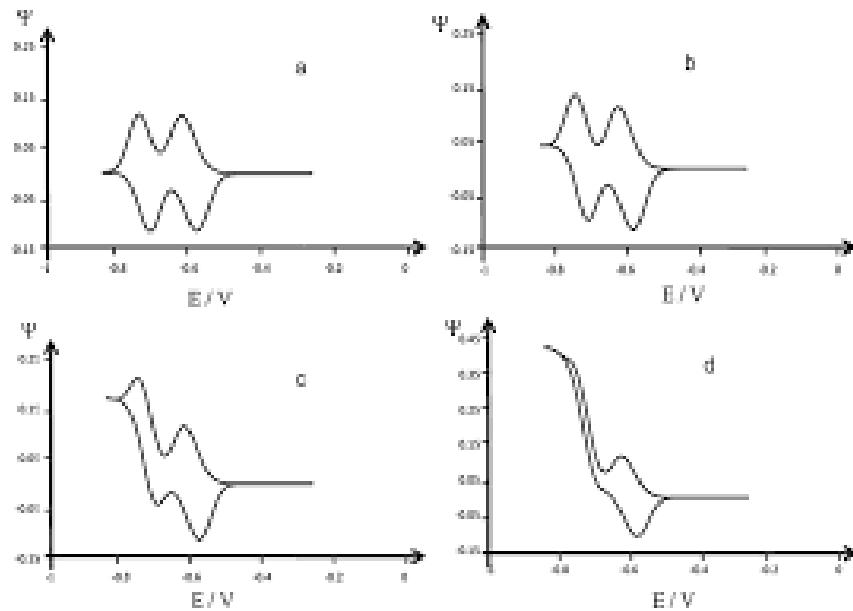
Fig. 1 Schematic illustration depicting a single redox cycle.











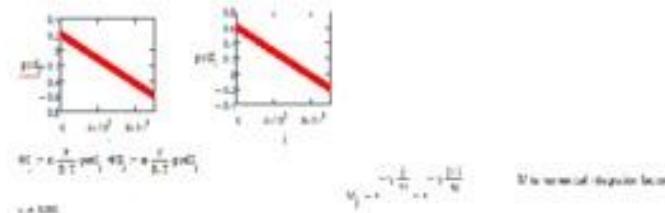
SUPPLEMENTARY MATERIAL: MATHCAD FILE for TWO-STEP SURFACE EECrev MECHANISM

(a) reaction mechanism	$\alpha \rightarrow \beta$	(b) SW mechanism	$\gamma \rightarrow \beta$	$\beta \rightarrow \alpha$	$\delta \rightarrow \beta$
$\Delta G = 0.2$	$\Delta G = 0.1$	$\Delta G = 0.0$	$\Delta G = 0.1$	$\Delta G = 0.2$	$\Delta G = 0.1$
$\alpha = 1$	$E_0 = 20.0$	$E_0 = 12.0$	$E_0 = 20.0$	$E_0 = 12.0$	$E_0 = 12.0$
$\gamma = 1$	$\frac{dE}{dt} = 0$	$\frac{dE}{dt} = 0$	$\frac{dE}{dt} = \left(\frac{\ln(1-\beta)}{t}\right)$	$\frac{dE}{dt} = \left(\frac{\ln(1-\beta)}{t}\right)$	$\frac{dE}{dt} = \left(\frac{\ln(1-\beta)}{t}\right)$
$\beta = 1$	$\frac{dE}{dt} = 0$	$\frac{dE}{dt} = 0$	$\frac{dE}{dt} = 0$	$\frac{dE}{dt} = 0$	$\frac{dE}{dt} = 0$

where α is the standard reversible mechanism, β is the adsorbed intermediate, γ is the second-step mechanism, and δ is the desorption mechanism.

$$\text{prob}_{\alpha} = 1 - \alpha + \alpha e^{-\left[\left(\frac{E-E_0}{kT}\right)t + \frac{\ln(1-\beta)}{kT} + \left(\frac{\ln(1-\beta)}{kT}\right)(t-1)\right] - \theta}$$

$$\text{prob}_{\beta} = \alpha(1-\alpha)e^{-\left[\left(\frac{E-E_0}{kT}\right)t + \left(\frac{\ln(1-\beta)}{kT}\right) + \left(\frac{\ln(1-\beta)}{kT}\right)(t-1) - \theta\right]}$$



$$R_t = \frac{2}{3} \text{prob}_{\alpha} \text{prob}_{\beta} = \frac{2}{3} \alpha(1-\alpha)$$

$$V_t = -\sqrt{\frac{2}{3}} \frac{1}{\pi} \sqrt{1-t}$$

R_t is the overall desorption rate.
 V_t is the overall desorption bias.

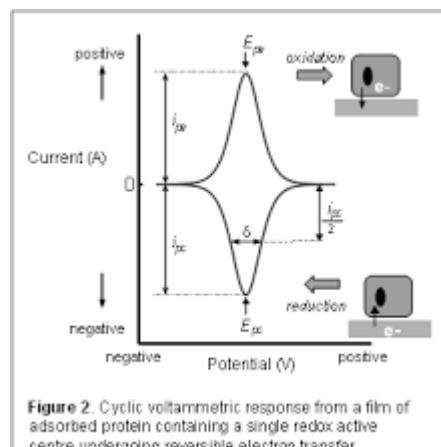
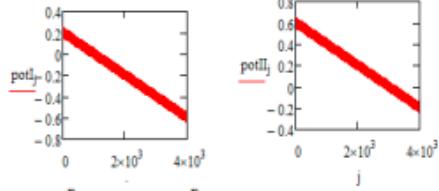


Figure 2. Cyclic voltammetric response from a film of adsorbed protein containing a single redox active centre undergoing reversible electron transfer.

$$\begin{aligned}
& \text{EsI} := 0.2 \quad \Delta E := 0.8 \quad dE := 0.01 \quad \text{Esw} := 0.05 \quad \text{EsII} := 0.6 \quad t := 1..1 \\
& n := 1 \quad F := 96500 \quad R := 8.314 \quad T := 298.15 \quad K_I := 10^0 r \quad K_{II} := 10^0
\end{aligned}$$

$$\begin{aligned}
j &:= 1.. \frac{\Delta E}{dE}, 50 \\
&\alpha_2 := 0.5 \\
&\text{pot}_{I,j} := \text{EsI} + \text{Esw} - \left[\left(\text{cell}\left(\frac{j-1}{25}, \frac{1}{2}\right) \cdot dE + \text{if}\left(\frac{\text{cell}\left(\frac{j}{25}\right)}{2} = \text{cell}\left(\frac{j-1}{25}, \frac{1}{2}\right), 1, -1\right) \cdot (\text{Esw} + \text{Esw}) \right) - dE \right] \\
&\text{pot}_{II,j} := \text{EsII} + \text{Esw} - \left[\left(\text{cell}\left(\frac{j-1}{25}, \frac{1}{2}\right) \cdot dE + \text{if}\left(\frac{\text{cell}\left(\frac{j}{25}\right)}{2} = \text{cell}\left(\frac{j-1}{25}, \frac{1}{2}\right), 1, -1\right) \cdot (\text{Esw} + \text{Esw}) \right) - dE \right] \\
&\alpha_1 := 0.5 \\
&\log(K_I r) = 0 \\
&K_{III} := 0.1 \\
&z := 2
\end{aligned}$$



$$\Phi I_j := n \cdot \frac{F}{R \cdot T} \cdot \text{pot}_{I,j} \quad \Phi II_j := n \cdot \frac{F}{R \cdot T} \cdot \text{pot}_{II,j}$$

$$k := 1.. \frac{\Delta E}{dE}, 50$$

$$S_k := e^{\frac{z}{50}(-k)} - e^{\frac{z}{50}(-k+1)}$$

TWO STEP SURFACE CEE MECHANISM MATHEMATICAL MODEL IN SQUARE WAVE VOLTAMMETRY

KI and KII are kinetic parameters related to the first and second electron transfer step
alpha is the electron transfer coefficient
EsI and EsII are potentials related to the first and the second electron transfer step
n is number of electron exchanged
F is Faraday constant
Esw is SWV amplitude
T is temperature
dE is potential step
Phi is dimensionless potential
Psi is dimensionless current
K is equilibrium constant -Keq
z is dimensionless chemical parameter-Kchemical = epsilon

$$\begin{aligned}
x &:= 0.001 \\
\Psi_{I,r} &:= \text{root} \left[\frac{\frac{K_I r e^{-\alpha_1 \cdot \Phi I_1} \cdot K}{1+K} \left(1 - \frac{1}{50} \cdot 0 \right) - (z)^{-1} K_I r \left(\frac{1}{1+K} \right) (-1) \cdot e^{-\alpha_1 \cdot \Phi I_1} \cdot 0 - \frac{K_I r}{50} \cdot e^{\Phi I_1 \cdot (1-\alpha_1)} \cdot 0}{\frac{K_I r e^{-\alpha_1 \cdot \Phi I_1} \cdot K}{1+K} \cdot \frac{1}{50} + 1 + (z)^{-1} K_I r \cdot (-1) \cdot \left(\frac{1}{1+K} \right) S_1 \cdot e^{-\alpha_1 \cdot \Phi I_1} + \frac{K_I r}{50} \cdot e^{\Phi I_1 \cdot (1-\alpha_1)}} \right] \cdot (1+0) \\
&x = \frac{K_I r}{50} \cdot e^{(1-\alpha_1) \cdot \Phi I_1} \left[\frac{x \frac{K_{II} e^{-\alpha_2 \cdot \Phi II_1}}{50}}{1 + \frac{K_{II} e^{-\alpha_2 \cdot \Phi II_1}}{50} \cdot (1 + e^{\Phi II_1})} \right] - K_I r \cdot e^{-\alpha_2 \cdot \Phi II_1} \cdot x \\
\Psi_{II,r} &:= \frac{\frac{K_{II} e^{-\alpha_2 \cdot \Phi II_1}}{50}}{1 + \frac{K_{II} e^{-\alpha_2 \cdot \Phi II_1}}{50} \cdot (1 + e^{\Phi II_1})}
\end{aligned}$$

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