

# Tekstilna industrija

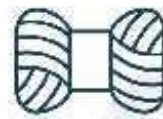


1868 - 2019

SAVEZ INŽENJERA I TEHNIČARA TEKSTILACA SRBIJE  
UNION OF TEXTILE ENGINEERS AND TECHNICIANS  
OF SERBIA



THIMBLE



Naučni i stručni časopis tekstilne i odevne industrije

Scientific and professional journal of the Union of textile engineers and technicians of Serbia



TAILOR'S DUMMY



SPOOL



IRON



CROCHET



LEATHER



JACKET



SEWING PATTERN



CROSS-STITCH



BOBBIN



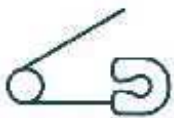
TAILOR'S SHEARS



KNITWEAR



BUTTONS



SAFETY PIN



KNITTING



BOWKNOT



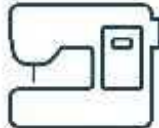
CLOTHING



MEASURING TAPE



DRESS SHIRT



SEWING CASE

CLOTH

SEWING MACH

Najbolja  publikacija za 2018. godinu





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Војске Југославије 12 , 192 10 Бор

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1868 - 2019

# tekstilna industrija

Naučni i stručni časopis tekstilne industrije UDK 677+687 ISSN 0040-2389  
Scientific and professional journal of the Union of textile engineers and technicians of Serbia

Volume LXVII • Number 4 • Beograd 2019 • Page 1-88 • Printing 100  
Publisher: Textile Engineers and Technicians Union of the Republic Serbia  
Editorial offices: Serbia, 11000 Beograd, Kneza Miloša 7a/II, tel: 064 15 03 053  
e-mail: casopistekstilnaindustrija@gmail.com

For publisher: Snežana Urošević, Ph.D.

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<b>THE MINISTRY OF EDUCATION, SCIENCE AND TECHNOLOGICAL DEVELOPMENT PARTICIPATED IN FINANCING OF THE JOURNAL</b>	

## REČ UREDNIKA

Svake godine potrošači troše ogromne količine novca na odeću. Svakodnevno se kupuju komadi koji su prekopotrebni, ali i oni odevni predmeti koji će privremeno pružiti zadovoljstvo potrošaču. Međutim, postavlja se pitanje koliko puta pri kupovini pogledamo deklaraciju? Koliko puta se zapitamo koja je sirovi- na upotrebljena za željeni odevni predmet? U većini slučaja odgovor je -retko, a možda i -nikad. To je samo jedan dokaz neodgovornog ponašanja potrošača. Ali, zašto bi potrošači morali da vode računa ko, gde i na koji način proizvodi odevne predmete?

Potrošači kupuju onda kada osete potrebu ili želju za nekim odevnim predmetom. Na odluku potro- šača utiču brojni aspekti poput društvenih, ekonomskih, socioloških, a koji igraju glavnu ulogu pri njego- vom konačnom izboru. Potrebno je zapitati se, da li su potrošači upoznati sa pojmom društveno odgovor- nog ponašanja.

Glavni problem nastaje onda kada istraživanjem dođemo do zaključka da većina potrošača i kupaca nisu upoznati sa pojmom društvene odgovornosti i društveno odgovornog poslovanja. Kupci navode da im kriterijum društveno odgovornog poslovanja nije bitan prilikom biranja i kupovine odevnih predmeta, kao i da ne bi platili proizvode više, ukoliko bi isti zadovoljavali kriterijum društvene odgovornosti. Većina potrošača više pažnje obraća na kvalitet i karakteristike proizvoda u smislu cene.

Na jednu stranu, potrošačima je bitno da predmet bude izrađen od prirodnih materijala i da nije testi- ran na životinjama, ali isto tako bi pre kupili odevni predmet od prirodnog krzna nego veštačkog. Samim tim, vidljivo je da kupci ne znaju i nisu svesni u potpunosti šta je to društvena odgovornost. Oni takođe nisu svesni globalnog problema, koje oni svojim neodgovornim ponašanjem čine za okolinu, zajednicu i društvo.

Većina poznatih kompanija danas pokušava da implementira društvenu odgovornost u svoje poslo- vanje. One ulažu mnogo napora da budu odgovorniji prema svojim zaposlenima i da proizvode i nabavlja- ju svoje resurse od dobavljača koji poštuju njihove zahteve. Takođe, sve veći broj preduzeća vodi računa o odnosu prema potrošačima, naročito u oblastima gde je jaka konkurencija, na svim proizvodima su prisut- ne jasne deklaracije o sadržaju i karakteristikama proizvoda.

Međutim, situacija u Srbiji i nije tako idealna. Praksa društveno odgovornog poslovanja je nedovoljno razvijena, osim malog broja preduzeća, koja vode računa o uticaju svog poslovanja na društvo i prirodnu sredinu i izveštavaju o efektima tih aktivnosti, daleko veći broj preduzeća doprinosi daljem širenju i produ- bljivanju socijalnih i ekoloških problema.

Glavni i odgovorni urednik  
Prof. dr Snežana Urošević

# SELECTION OF FUSIBLE INTERLINING IN APPAREL INDUSTRY

Sashka Golomeova Longurova<sup>1</sup>, Goran Demboski<sup>2</sup>, Sonja Jordeva<sup>1</sup>,  
Silvana Zezova<sup>1</sup>, Vangja D. Kuzmanoska<sup>1</sup>, Marija Kertakova<sup>1</sup>, Kiro Mojsov<sup>1</sup>

<sup>1</sup> Faculty of Technology, University „Goce Delcev“ – Shtip,  
Krste Misirkov 10-A, Shtip, N. Macedonia  
\* e-mail: saska.golomeova@ugd.edu.mk

<sup>2</sup> Faculty of Technology and Metallurgy, University „St. Kiril and Metodij“ - Skopje

**Naučni rad**

UDC: 687.053.665:677.074.33

doi: 10.5937/tekstind1904004G

**Abstract:** *The purpose of this paper was to select a fusible interlining in the production of men's shirts. The selection was based on bonding strength between the fabric and the interlining as a key property that defines the quality of the fusible interlining. The bonding strength was examined after fusing process and after five cycles of laundering. The fabric was fused with three fusible interlinings from different manufacturers and with different properties.*

**Key words:** fusible interlining, bonding strength, orthogonal array.

## SELEKCIJA TERMOPLASTIČNE MEĐUPOSTAVE U INDUSTRIJI ODEĆE

**Apstrakt:** *Cilj ovog rada je selekcija termoplastične međupostave u proizvodnji muških košulja. Selekcija se zasniva na jačini spoja između tkanine i međupostave kao ključne karakteristike koja određuje kvalitet termoplastične međupostave. Jačina spoja ispitivana je nakon postupka fiksiranja i nakon pet ciklusa pranja. Za termofiksiranje tkanine korišćene su tri različite međupostave, različitih proizvođača i različitih karakteristika.*

**Ključne reči:** Termoplastična međupostava, jačina spoja, ortogonalni niz.

### 1. INTRODUCTION

Fusible interlinings are auxiliary materials in apparel production and they are very important for essential apparel quality. Fusible interlinings reinforce the fabric, improve the formability and tactile properties of outer fabric, and give a beautiful silhouette of the apparel [1,2,3]. With the fusing process, fusible interlining is bonded to the outer fabric by thermoplastic resin and produces a structure called laminate [4]. The bonding strength between the interlining and the fabric is very important for apparel quality because consumers want to keep the shape of apparel during wearing and after repeated laundering. During the wearing and laundering, apparel is exposed to mechanical stress and may cause delamination of

the fusible interlining, which may impair the aesthetic appearance of the fused parts of the apparel. The bonding strength between the fusible interlining and outer fabric is essential for obtaining a laminate that will stand the process of laundering and dry cleaning. Although the minimum bond strength is not specified in the standards for bonding strength testing, in the literature and from practical experience, data can be found that the bond strength should be at least 10 N / 5cm or 200 cN / cm [5]. Factors which have influence on the bonding strength of the laminate are fusible interlining and the parameters of fusing process, pressure, temperature and time.



## 2. EXPERIMENT

In this paper, bonding strength was investigated between one fabric intended for men's shirts and three different fusible interlinings. The structural characteristics of the fabric and fusible interlinings are given in Table 1 and in Table 2, appropriate.

**Table 1:** Specification of fabric

Raw material	100% cotton
Weight, g/m <sup>2</sup>	125
Warp density ,cm <sup>-1</sup>	56
Weft density, cm <sup>-1</sup>	38

**Table 2:** Specification of fusible interlinings

		Fusible interlining		
		Freudenberg	Wendler	Staflex
Weight, g/m <sup>2</sup>		80	100	110
Composition	Substrate	100% cotton, woven	100% cotton, woven	100% cotton, woven
	Thermoplastic resin	PEHD, micro dots	PEHD, micro dots	PEHD, micro dots
Fusing parameters	T, °C	143-166	160-165	150-170
	P, bar	0,8-3	2-3	1,8 – 2,5
	t, s	12-18	12-18	12-17
Care	T <sub>max</sub> laundering, °C	95	95	95
	T <sub>max</sub> ironing, °C	150	150	150

Using orthogonal array L<sub>9</sub> (3<sup>4</sup>) the experiment plan was made, as shown in Table 3. The experiments were carried out with 4 factors (A- fusing interlining; B- Temperature, C- pressure, D-time) at 3 levels, as shown in Table 4. Selection of the levels is based on the interlining fusing parameters specifications. The experiment layout using an "L<sub>9</sub>" orthogonal array in Table 5 is shown.

**Table 3:** "L<sub>9</sub> (3<sup>4</sup>)" orthogonal array

Factors				
	A	B	C	D
1	1	1	1	1
2	1	2	2	2
3	1	3	3	3
4	2	1	2	3
5	2	2	3	1
6	2	3	1	2
7	3	1	3	2
8	3	2	1	3
9	3	3	2	1
L <sub>9</sub> (3 <sup>4</sup> )				

**Table 4:** Factors and levels

Factors	Levels		
	I	II	III
Fusing interlining(A)	Freudenberg	Wendler	Staflex
Temperature (B)	150 °C	160 °C	170 °C
Pressure (C)	1 bar	2 bar	3 bar

**Table 5:** Experiment layout using an "L<sub>9</sub>" orthogonal array table

Exp.no	Factor and level			
	A	B	C	D
1	Freudenberg	150	1	12
2	Freudenberg	160	2	15
3	Freudenberg	170	3	18
4	Wendler	150	2	18
5	Wendler	160	3	12
6	Wendler	170	1	15
7	Staflex	150	3	15
8	Staflex	160	1	18
9	Staflex	170	2	12

The three types of fusible interlinings were taken as levels of the factor A - fusible interlining. At the Level 1 is interlining produced by Wendler, Germany, level 2 interlining produced by Staflex, Spain and

level 3 is interlining produced by Freudenberg, Germany. The fusing process was carried out in factory conditions, on continuous fusing press type Gygli. Six samples were fused at each fusing conditions. Half of the samples, after fusing were exposed to five cycles of laundering and drying according the conditions in given in the ASTM D 2724 standard. After the fifth cycle, the samples were placed in a flat position on a flat surface and hand-ironed at 150°C. During ironing no extra pressure was applied except the mass of the iron itself. The bonding strength of the fused laminate was tested on tensile testing machine Tinius Olsen HT45, in accordance with the ASTM D 2724 standard [7].

### 3. RESULTS AND DISCUSSION

The obtained results for bonding strength investigated after fusing process and after five cycles of laundering are given in Figure 1. The results given on the diagram calculate average values from the three measured values. According to the results, the highest bonding strength indicates the „Freudenberg“ interlining, followed by „Staflex“ interlining, while the lowest bonding strength indicates interlining produced by „Wendler“. Compared to the minimum bonding strength of 200 cN/cm, generally laminates with interlinings „Freudenberg“ and „Staflex“, have required bonding strength. The „Wendler“ laminate, in all cases shows lower strength than 200 cN/cm.

The „Freudenberg“ laminate, for all combinations of parameters, after fusing process as after laundering process, has a higher values of bonding strength between fabric and interlining than the minimum strength of 200cN/m. The bonding strength of this laminate increases with the fusing parameters (temperature, pressure and time) increasing. Comparison of the values of the bonding strength after fusing and after 5 cycles of laundering indicates that the bonding strength after five cycles of laundering is higher than the strength after fusing, for all combination of parameters. According to the literature after laundering, the bonding strength decreases, but after ironing, as in our case, the strength may increase [6]. After ironing, the increasing of bonding strength is the result of the consolidation of the thermoplastic resin due to the effect of temperature and the pressure in the ironing process.

In the both cases of examination, after fusing process and after laundering process, for all combinations of fusing parameters, the „Wendler“ laminate has lower bonding strength values than the minimum strength of 200 cN /cm. The results of samples tested after fusing process, showed that the bonding strength increases with the rising of the temperature.

The obtained results show that the bonding strength after five cycles of laundering is lower than the bonding strength after fusing process, for all combinations of parameters.

The „Staflex“ laminate, for all combinations of parameters, has a higher bonding strength than 200cN/cm for samples tested after the fusing process. After five cycles of laundering, the value of bonding strength is slightly below 200cN/cm except for the sample fused at the highest temperature of 170 °C. With rising of the temperature, the bonding strength slightly decreases in the group of samples tested after fusing. In the group of samples examined after laundering happens the opposite, the bonding strength increases with raising of the temperature.

In general, the comparison of the results of the bonding strength after fusing and after five cycles laundering indicates that the bonding strength decreases after laundering.

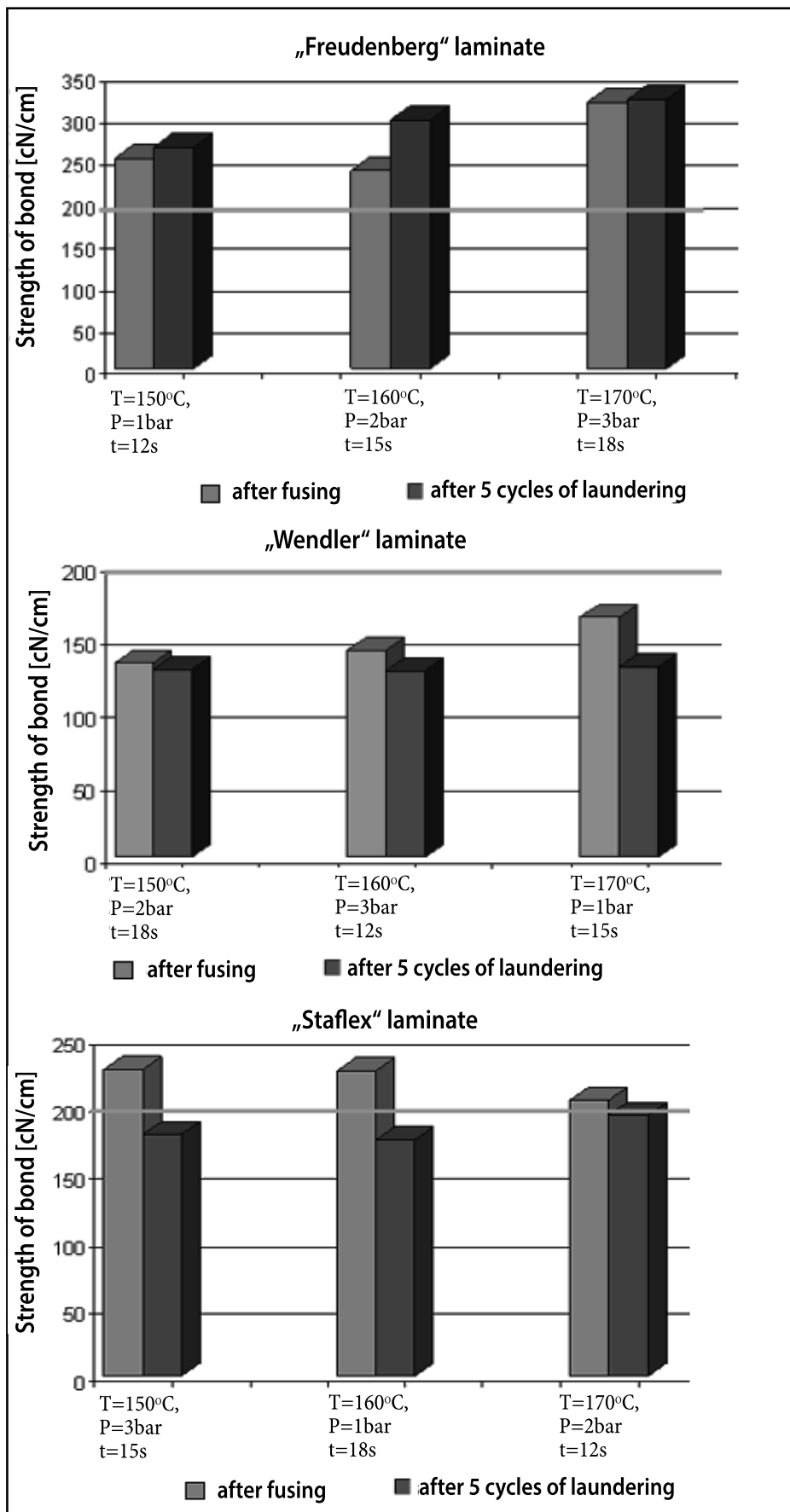
In the Figure 2 standard deviation of bonding strength for three types of fusible interlinings at all fusing parameters are shown.

From Figure 2, can be seen that the standard deviation of the bonding strength for the „Freudenberg“ laminate is significantly changed by fusing parameters variation. In general, „Freudenberg“ interlining shows that with increasing of the temperature the standard deviation increases for all samples, except for samples fused at temperature 170 °C and tested after the fusing process. Here, for the highest fusing temperature 170 °C the standard deviation is slightly lower than that of temperature 160 °C. From Figure 1 we have seen that at higher temperature the bonding strength is higher, but it can be noticed that the standard deviation, i.e. the coefficient of variation is increased, which must be taken into account when the optimal fusing parameters are being chosen.

The standard deviation of bonding strength of the fabric and interlining in the „Wendler“ laminate doesn't show any trend in the magnitude under different fusing conditions. In the group of samples tested after fusing process, the sample fused at the lower temperature (150 °C) shows the lower standard deviation of the bonding strength than at the higher fusing temperatures. Samples tested after five cycles of laundering generally show higher standard deviation than samples examined after fusing process; higher at temperatures of 150 °C and 170 °C and lower at the temperature of 160 °C.

Standard deviation of bonding strength in the „Staflex“ laminate increases with fusing temperature increasing for all examined samples (Figure 2). Sam-





**Figure 1:** Bonding strength of the laminate after fusing and after five cycle of laundering

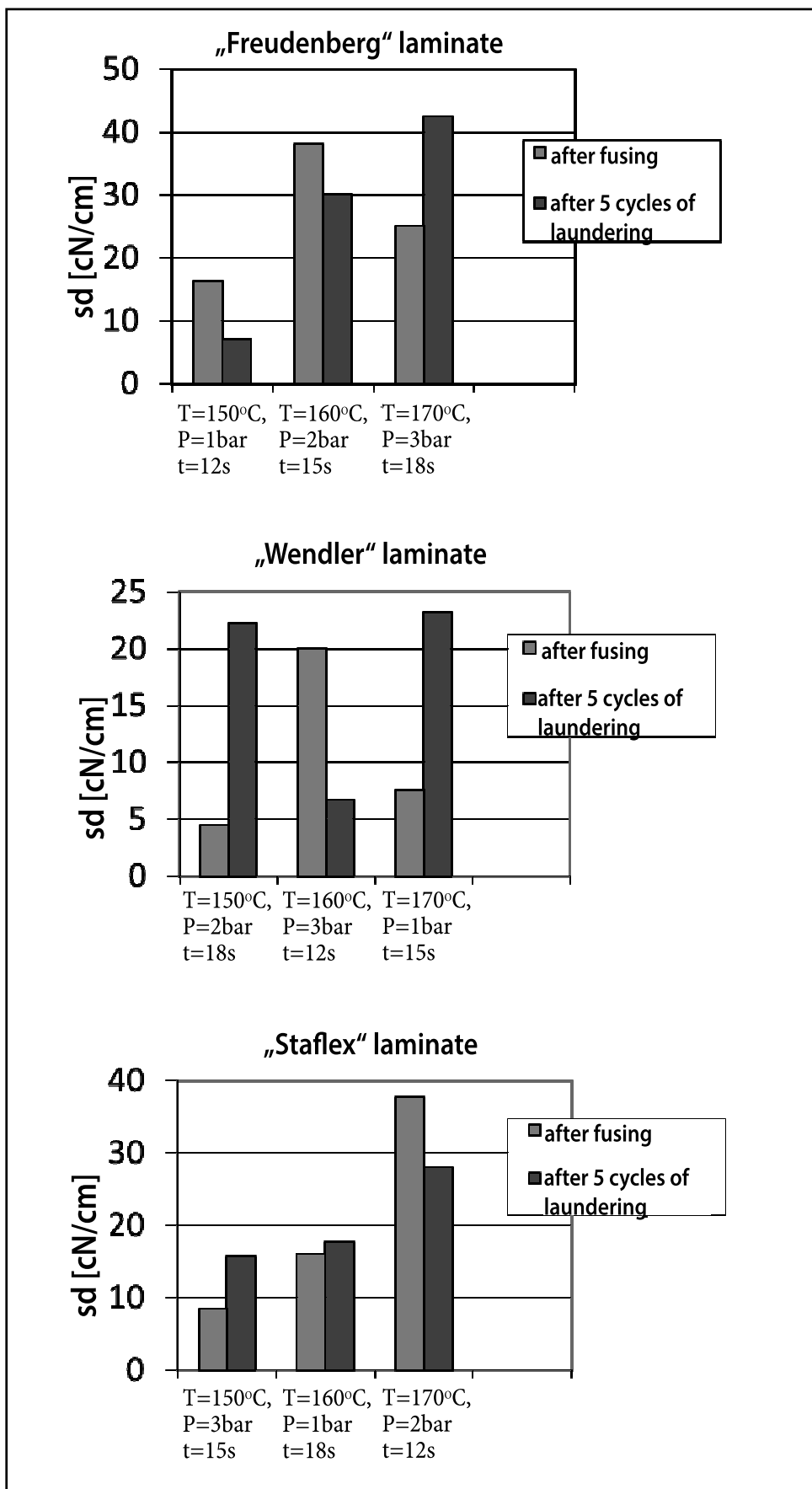


Figure 2: Standard deviation of bonding strength for all applied fusing parameters

ples tested after laundering, fused at temperatures 150 °C and 160 °C, show higher standard deviation of bonding strength than the samples tested after fusing process. In the case of this interlining, at the highest temperature the highest bonding strength is not obtained (Figure 1) which may suggest that it is more advantageous to use a lower temperature in terms of higher bonding strength, lower standard deviation and energy savings.

In consideration of the information given in the technical specification of interlinings, comparison of the obtained results of bonding strengths for different fusible interlinings leaves us some doubts. If we remind on table 2 with the recommended fusing parameters for the interlinings, it is noted that interlining by the manufacturer "Freudenberg" has the smallest weight (80 g/m<sup>2</sup>), and consequently (assuming that the participation of the thermoplastic resin is approximately equal for all interlinings) the smallest amount of thermoplastic resin. However, this fusible interlining shows the higher bonding strength. Next, it is "Staflex" interlining which has highest weight (110 g/m<sup>2</sup>) and the last is "Wendler" interlining with a weight of 100 g / m<sup>2</sup>. A possible explanation for the higher bonding strength of the "Freudenberg" laminate may be in the range of recommended fusing temperatures in the interlining specification (table 2) given by the manufacturer. Compared to other interlinings, the temperature range recommended by this manufacturer (143-166 °C) is quite wide ( $\Delta T = 23$  °C), and the initial fusing temperature is also lower (143 °C). Also, the fusing temperature recommended by this manufacturer is from 0.8 to 3 bar ( $\Delta P = 2.2$  bar), which is quite low initial pressure and widest fusing pressure range compared to other interlinings. The comparison of these parameters with the fusing parameters applied in the experiment (table 4), shows that especially at the third level of the experiment (temperature of 170 °C and pressure of 3 bar) where the highest bonding strength were achieved, fusing temperature and pressure which are much higher than initial ((temperature of 143 °C and pressure of 0.8 bar) were used. Consequently, in this case it is possible extremely high mobility of the thermoplastic resin and improved penetration of the resin into the substrate and the base material to achieve due to the combination of higher temperature and higher pressure.

From the process economics point of view, lower levels of fusing parameters ( $T = 150$  °C,  $P = 1$  bar,  $t = 12$  s or  $T = 160$  °C,  $2$  bar,  $t = 15$ s) can be taken as optimal fusing parameters for the "Freudenberg" interlining because the bonding strength under these

conditions after the fusing process and after laundering is acceptable and the standard deviation is lower.

The interlining „Wendler“, which creates laminate with the lowest bonding strength, has the lowest fusing temperature range (160-165°C) recommended by the manufacturer. It could be thought that getting out of the narrow temperature range is a possible reason for very low bonding strength. Although, the fusing process was carried out with temperature of 160°C and pressure and time that completely overlap with recommended parameters from the specification, the laminate with this interlining has the lowest bonding strength compared to other fusible interlinings. The reason for this may be the low quality of thermoplastic resin, for which at the time of order and through the information available in the technical specifications no more detailed information can be found. In order to investigate the quality of the thermoplastic resin it is necessary to carry out tests which are not within the scope of the technical equipment of the apparel manufacturer.

#### 4. CONCLUSION

In this study, a selection of a fusible interlining in the production of men's shirts was made. From the obtained results we can conclude that:

1. Only "Freudenberg" interlining creates a laminate with a bonding strength higher than 200cN/cm in both cases, after fusing process and after five cycles of laundering. This result was obtained for all applied combinations of fusing parameters.
2. Fusing parameters in the specification of the "Freudenberg" interlining, temperature (143°C) and pressure (0,8 bar), are much more lower than the fusing parameters used in experiment and due to combination of the higher temperature and pressure, the viscosity of the thermoplastic resin decreases and penetration of the resin into the substrate and the outer fabric is improved.
3. When temperature and pressure are increasing, the bonding strength increases and standard variation increases, too.
4. For "Freudenberg" interlining fusing we suggest the lower fusing parameters ( $T= 150^{\circ}\text{C}$ ,  $P=1\text{bar}$ ,  $t=12\text{s}$ ) because the bonding strength is acceptable and the standard deviation is the lowest.

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Rad primljen: 18.11.2019.

Rad prihvaćen: 9.12.2019.