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Miami, Florida, USA, November 13–16, 2016

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Message From the CEFC Editor-in-Chief

THE 17th Biennial IEEE Conference on Electromagnetic Field Computation (IEEE-CEFC) was held in Miami, Florida, USA, from November 13 to 16, 2016. The conference's technical program attracted 916 digests from 35 countries. Once again, the large number of high-quality scientific contributions confirms that CEFC remains among the foremost conferences for the computational electromagnetics community.

The IEEE-CEFC 2016 activities constituted an excellent forum for specialists from academia, research centers, and industry worldwide to establish cooperation and share knowledge and experience, and for the cross-fertilization of new ideas in the design, analysis, innovative media utilization, and optimization methods for electromagnetic devices. The main topics were Static and Quasi-static Fields, Wave Propagation, Material Modeling, Coupled Problems, Numerical Techniques, Optimization and Design, Software Methodology, Nanomagnetics, Nanophotonics, Bioelectric Field computation, as well as Devices and Applications.

It is worth noting that the review process was performed in two stages. The Editorial Board Chairman/Editor-in-Chief first invited qualified experts on the above fields to become members of IEEE-CEFC 2016 Editorial Board as associate editors. In the subsequent stage, the associate editors assigned each digest to at least two reviewers selected based on their expertise. A score-based review procedure was used for the selection of accepted digests. The score ranged from 1 to 10 and was used to evaluate relevance, originality, quality, significance of results, language clarity, and technical presentation. As a result of implementing this peer review process, 588 digests were accepted and presented at the conference. An additional note relating to the technical program of the conference is that three prizes (U.S. $500 each) were awarded for best poster presentation to young researchers who participated in IEEE-CEFC 2016 during the closing ceremony.

After the conference, authors of accepted digests were invited to submit an extended four-page versions of their papers to the IEEE TRANSACTIONS ON MAGNETICS. As a result, 479 papers were submitted. An International Editorial Board comprising the Editor-in-Chief and 19 associate editors handled the review process for the extended version:

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19) Yang, Shiyou (China).

Each of the associate editors assigned papers to reviewers, following the standard IEEE TRANSACTIONS review process. As a result, each paper had at least two peer reviews. Some papers went through a second or even a third review cycle. At the end of this process, 242 papers were accepted for publication in this issue of IEEE TRANSACTIONS ON MAGNETICS. We hope the reader of this issue finds these papers to be intriguing and of high scientific quality.

In closing, I would like to note the excellent organization and management skills of the Conference Chair Prof. Osama Mohammed that made this conference a success. In addition, I would like to express my sincere appreciation to the authors and all the participants whose high-level contributions guaranteed the success of IEEE-CEFC 2016. Moreover, I would like to affirm my gratitude to the associate editors and the reviewers for their diligent work throughout the peer review process.

A. A. ARKADAN, *Editor-in-Chief*
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A New Adaptive Mesh Refinement Method in FEA Based on Magnetic Field Conservation at Elements Interfaces and Non-conforming Mesh Refinement Technique

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Mesh quality strongly affects the solution accuracy in electromagnetic finite element analysis. Hence, the realization of adequate mesh generation becomes a very important task. Several adaptive meshing methods for automatic adjustments of the mesh density in accordance with the shape and complexity of the analyzed problem, have been proposed. However, the most of them are not enough robust, some are quite laborious and could not be universally used for adaptive meshing of complex analysis models.

In this paper, a new adaptive mesh refinement method based on magnetic field conservation at the border between finite elements is proposed. The proposed error estimation method provides easy mesh refinements, generates smaller element within regions with large curvature of the magnetic flux lines. The proposed adaptive mesh refinement method based on non-conforming edge finite elements, which could avoid generation of flat- or ill-shaped elements, was applied to a simple magnetostatic permanent magnet model. To confirm the validity and accuracy, the obtained results were compared with those obtained by means of the Zienkiewich-Zhu (ZZ) error estimator. The results show that the computational error using the proposed method was reduced down to 1.0% compared with that of the ZZ method which yields error of 8.6%, for the same model.

***Index Terms*—Adaptive meshing, element surface integral term, error estimation, finite element analysis.**

I. Introduction

Finite element method (FEM) is one of the most successful numerical simulation methods in electromagnetics. However, an eternal problem is how to generate adequate mesh to enhance simulation accuracy, and reduce computation time and used memory. Hence, to tackle this problem, some adaptive meshing techniques have already been investigated [1], [2].

Two major techniques are required for obtaining good adapting meshing method: (1) a good error estimation method, and (2) an adequate mesh refinement technique, of which the first one has crucial importance. Although the Zienkiewicz-Zhu (ZZ) method [3] is widely used as an error estimator, recently some other error estimation methods based on the local (element) error estimators obtained from the local verification (residual) of the FEM analysis and the conservation of the magnetic field $\boldsymbol{H}$ at the interface between two elements are very promising [4]–[6]. These newly introduced error estimator have proven superior to the ZZ method, pointing out that the magnetic field conservation could be successfully used as an error estimator in FEM analysis. However, no results have already been reported on a development of an adaptive FEA using this superior error estimator based on the magnetic field conservation.

Mesh refinement scheme is also important in an adaptive meshing. After estimation of the errors, elements estimated to have a large error need to be refined. As a mesh refinement technique for triangular or tetrahedral meshes, the Delaunay triangulation method is conventionally used. However, using the Delaunay triangulation method, many ill-shaped elements such as flat, distorted, or inside-out elements are generated. Therefore, we proposed a new mesh refinement method using the non-conforming finite element technique [7], [8].

In this paper, the authors proposed a new adaptive meshing method based on the magnetic field conservation between two elements and the non-conforming edge finite element technique. The proposed method results with a generation of a suitably coarse mesh with less number of finite elements and less computational cost.

II. Adaptive Meshing Method

A. Adaptive Meshing Method

Fig. 1 shows the flow of common adaptive meshing finite element analysis (FEA). A bad error estimator could lead to generation of an unnecessary large number of elements with low accuracy result. Nevertheless, a good error estimator produces a fine mesh with adequately large and well distributed finite elements, resulting with high accurate

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computational results.

The commonly used ZZ error estimator [3] performs error estimation based on the field energy:

$$\lambda_e = \frac{\frac{1}{2}\int (\boldsymbol{B}_e - \bar{\boldsymbol{B}}_e)\cdot \nu(\boldsymbol{B}_e - \bar{\boldsymbol{B}}_e)\,\mathrm{d}e}{\frac{1}{2}\int \bar{\boldsymbol{B}}_e \cdot \nu \bar{\boldsymbol{B}}_e\,\mathrm{d}e} \tag{1}$$

where λ_e, $\boldsymbol{B}_e$, $\bar{\boldsymbol{B}}_e$, and ν are the estimated error, the magnetic field obtained from FEA, the magnetic field estimated from the neighboring elements, and the magnetic reluctivity, respectively. Although the ZZ method is a very good error estimator, often in the air region far from objects, this method results with gratuitously subdivided smaller elements (*e.g.* Fig. 7(c)), that unwontedly increase the number of elements and the computational time, while in the same time, does not improve the computational accuracy.

As seen from Fig. 1, the mesh improvement procedure is the second important task for obtaining highly accurate solutions. Commonly, the Delaunay triangulation method is used for mesh improvement. It is a well-known, stable, and powerful tool for making triangular or tetrahedral meshes. However, when it is used for mesh refinement in an adaptive FEA, many ill-quality elements are generated. As shown in Fig. 2, even if the shapes of a parent element is well, after subdivision, newly generated offspring elements become ill-shaped, or if a flat parent element is subdivided, flatter offspring elements are generated. Subsequently, with each subsequent subdivision, the quality of elements downgrades, making the Delaunay triangulation method unsuitable for the mesh improvement in an adaptive FEA.

Therefore, in this paper we implemented a new adaptive analysis method which utilizes a new error estimator based on the magnetic field conservation on the interface between two elements [4], and a new mesh refinement scheme based on the non-conforming edge-based FEA [7], [8].

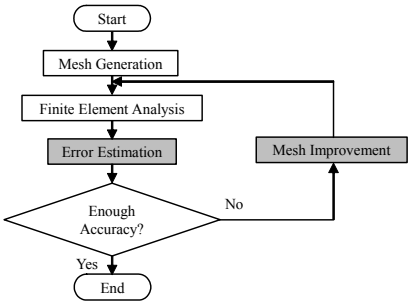

Fig. 1. Flowchart of conventional adaptive meshing FEA.

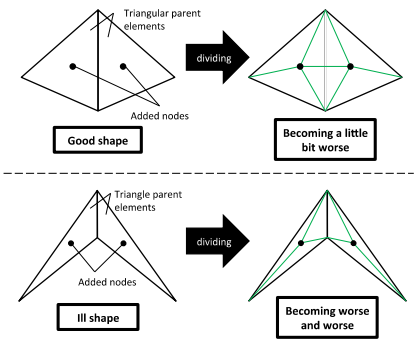

Fig. 2. Well-shaped parent element produce ill-shaped offspring elements (upper). Ill-shaped parent element produce ill-shaped offspring elements (lower).

B. Proposed Error Estimator based of the Magnetic Field Conservation

The governing equation for magnetostatic problems is:

$$\nabla\times(\nu\nabla\times\boldsymbol{A}) = \boldsymbol{J}_0 \tag{2}$$

where $\boldsymbol{A}$ and $\boldsymbol{J}_0$ are the magnetic vector potential and the source current, respectively. Applying the weighted residual method, from (2) the following equation could be obtained:

$$\int_v \boldsymbol{w}\cdot\nabla\times(\nu\nabla\times\boldsymbol{A})\,\mathrm{d}v = \int_v \boldsymbol{w}\cdot\boldsymbol{J}_0\,\mathrm{d}v \tag{3}$$

where $\boldsymbol{w}$ and v are the vector interpolation function and the integration volume, respectively. With integration by parts, the left term of (3) becomes:

$$\begin{aligned}&\int_v \boldsymbol{w}\cdot\nabla\times(\nu\nabla\times\boldsymbol{A})\,\mathrm{d}v \\ &= \int_v \nu(\nabla\times\boldsymbol{w})\cdot(\nabla\times\boldsymbol{A})\,\mathrm{d}v + \int_S \nu\boldsymbol{n}\cdot\left[(\nabla\times\boldsymbol{A})\times\boldsymbol{w}\right]\mathrm{d}S\end{aligned} \tag{4}$$

where S and $\boldsymbol{n}$ are the integration surface and the unit vector normal to the integration surface S, respectively.

In the formulization of edge-based FEM, the second term on the right side of (4) is neglected because the values of the tangential components of the magnetic field $\boldsymbol{H}$ should be regarded as identical on the interface between the adjacent two elements:

$$\int_S \nu\boldsymbol{n}\cdot\left[(\nabla\times\boldsymbol{A})\times\boldsymbol{w}\right]\mathrm{d}S = \int_S (\boldsymbol{H}\times\boldsymbol{w})\cdot\boldsymbol{n}\,\mathrm{d}S\,. \tag{5}$$

However, during the computation, these values slightly differ between each other. Therefore, one could use these differences as an error estimator in the adaptive meshing method.

Let us consider the elements i and j having the common interface S as shown in Fig. 3. This interface consists of the edges k, l, and m, and their vector interpolation functions $\boldsymbol{w}_k$, $\boldsymbol{w}_l$, and $\boldsymbol{w}_m$, respectively. Thus, the expression of the right term in (5) with respect to the edge k becomes:

$$d_{e,k} = \int_S (\boldsymbol{H}_e\times\boldsymbol{w}_k)\cdot\boldsymbol{n}_e\mathrm{d}S \quad (e=i,j)\,. \tag{6}$$

Similarly, two equations per edge could be written, while the following equations with respect to all three edges have to hold:

$$D_f = d_{i,f} + d_{j,f} = 0 \quad (f = k,l,m) \tag{7}$$

In the ordinary edge-based FEA, as a result of neglecting of the second right term in (4), the values for D_k, D_l, and D_m should be zero. However, in our case during the computation they are not zero and thus we utilize the calculated values for D_k, D_l, and D_m as an error estimator E_{ij} as following:

$$E_{ij} = \max\left(|D_k|,|D_l|,|D_m|\right) > \varepsilon \tag{8}$$

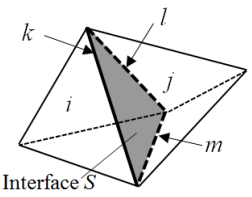

Fig. 3. The adjacent elements i and j with the common interface S. The triangular interface S consists of the edges j, k, and l.

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where ε is the prescribed threshold. If E_{ij} exceeds the threshold ε, the elements i and j are adaptively subdivided into smaller elements.

C. Proposed meshing refinement method utilizing non-conforming finite element technique

Let us suppose that an element has a large error as shown in Fig. 4(a), and it has to be subdivided into eight smaller finite elements. Obviously, the elements surrounding the element with large error remain unchanged, resulting in generation of non-conforming element surfaces between the elements. If the initial shape of the parent element before subdivision was well-shaped, then also the shapes of the newly generated eight finite elements could remain well-shaped.

Three kinds of non-conforming techniques have already been proposed: (1) the discontinuous Galerkin method [8], (2) the mortar FEM [9], and (3) the mesh interpolating method [10], and in this paper we use the third one.

In the non-conforming finite element technique, the vector potential on master edges is obtained from slave edges as shown in Fig. 4(b). The original FEA equation is:

$$\boldsymbol{K}\boldsymbol{a} = \boldsymbol{b} \tag{9}$$

where $\boldsymbol{K}$, $\boldsymbol{a}$, and $\boldsymbol{b}$ are the stiffness matrix, the vector potential, and the source vector, respectively. The vector potential on slave edges $\boldsymbol{a}$ has the following relation with that on the master edge $\tilde{\boldsymbol{a}}$:

$$\boldsymbol{a} = \boldsymbol{C}\tilde{\boldsymbol{a}} \tag{10}$$

where $\boldsymbol{C}$ is the constitutional matrix derived from the relation between the master and slave edges [10]. The following system of equations needs to be solved:

$$\boldsymbol{C}^{\mathrm{t}}\boldsymbol{K}\boldsymbol{C}\tilde{\boldsymbol{a}} = \boldsymbol{C}^{\mathrm{t}}\boldsymbol{b} \tag{11}$$

where t stands for transpose, and $\boldsymbol{C}^{\mathrm{t}}$ is introduced in order to generate a symmetrical stiffness matrix.

In the proposed adaptive meshing method, a several iterative steps are taken for mesh refinement until an error E_{ij} becomes below a defined tolerance value ε. Therefore, after the ith refinement iteration step the following system is derived:

$$\boldsymbol{C}_1^{\mathrm{t}}\cdots\boldsymbol{C}_i^{\mathrm{t}}\boldsymbol{K}_i\boldsymbol{C}_i^{\mathrm{t}}\cdots\boldsymbol{C}_1^{\mathrm{t}}\tilde{\boldsymbol{a}}_i = \boldsymbol{C}_1^{\mathrm{t}}\cdots\boldsymbol{C}_i^{\mathrm{t}}\boldsymbol{b}_i \tag{12}$$

where $\boldsymbol{C}_i$ is the constitution vector between the master and slave edges at the ith adaptive subdivision step. The system of linear equations (12) at the ith adaptive subdivision step needs to be solved, and the constitutional vectors $\boldsymbol{C}_j$ (j = 1, ⋯, i-1) of the previous steps could be reused to reduce a labor task. As for the stiffness matrix $\boldsymbol{K}_i$ and the source vector $\boldsymbol{b}_i$, it is just necessary to add their elements with respect to the newly subdivided elements to $\boldsymbol{K}_{i-1}$ and $\boldsymbol{b}_{i-1}$ at the previous step.

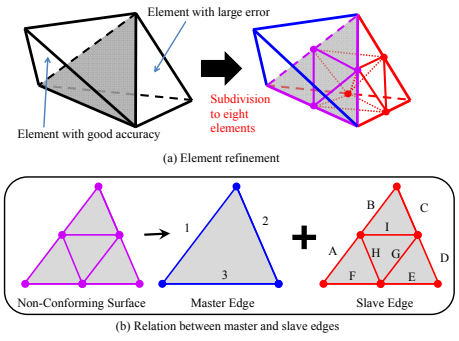

Fig. 4. (a) Subdivision of one element with large error to eight smaller elements, and (b) relation between master and slave edges on non-conforming surface.

The main features of proposed mesh refinement method are:

- Easier subdivision into smaller elements. Just one tetrahedral element is simply subdivided into eight tetrahedral elements with high shape quality.
- The matrix elements of newly generated elements on every adaptive step are only added to the constitutional vector, the stiffness matrix, and the source vector, while the constitutional vectors on the previous steps are reused.

After estimation of the computation error, it is not necessary to take into account the surfaces of objects during the mesh refinement procedure.

III. Application

To confirm the validity of the proposed adaptive method, we performed edge-based FEA on a simple model of a single permanent magnet (1T) as shown in Fig. 5, using a very rough tetrahedral initial mesh with 1325 elements. The mesh refinement behavior and accuracy transition of the proposed method were compared with those of the ZZ method. To keep approximately the same level of increasing rate of elements during mesh refinement for both, the proposed and the ZZ methods, only 10% of elements were allowed for subdivision per iteration.

A. Mesh refinement

In Figs. 6 and 7 the distribution of newly subdivided elements during iterative adaptive meshing process by the proposed and by the ZZ methods, respectively, are presented.

As shown in Fig. 6, the proposed method results into a finer mesh as expected mainly in the area around the permanent magnet. At earlier steps (Figs. 6(a) and (b)), the elements all over analysis area are subdivided. At the following steps (Figs. 6(c) and (d)), only finite elements belonging to the permanent magnet region and the air region surrounding the permanent magnet are evaluated. At the final step, only the elements near the outside surfaces of permanent magnet and the air are subdivided. Throughout the refinement process with the proposed method, only elements belonging in the area with large magnetic field gradient are chosen for subdivision.

In comparison, in case of the ZZ method the air region elements are subdivided in each step throughout the entire refinement process, as can be seen in Fig. 7. At the first step, the elements all over the analysis region are subdivided. However, at the second step, some elements on the top and

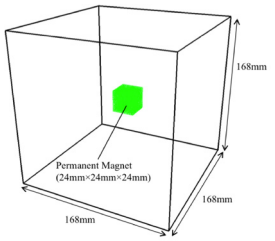

Fig. 5. Simple model of a single permanent magnet (1T).

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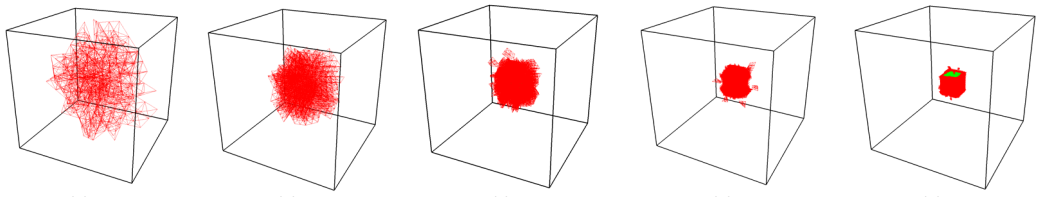

Fig. 6. Element subdivision map as the adaptive step proceeds in the proposed adaptive meshing method. The red-highlighted elements mean subdivided elements at each refinement step.

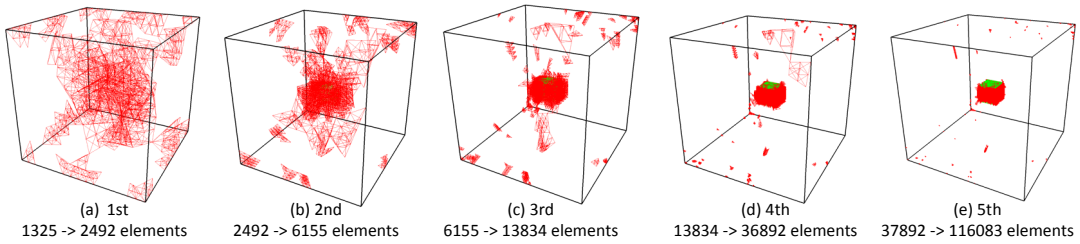

Fig. 7. Element subdivision map as the adaptive step proceeds in ZZ method. The red-highlighted elements are subdivided elements at each refinement step.

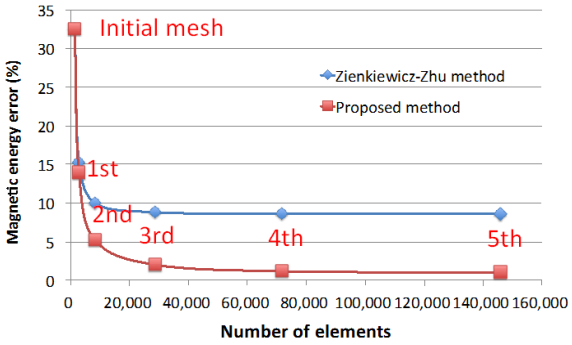

Fig. 8. Transition of magnetic field energy with increase of the number of elements in cases of the proposed adaptive meshing and ZZ method.

bottom surfaces and corners of analysis region are also evaluated as elements with large error, and consequently considered as a subject for subdivision. Even more, at the 3rd, 4th, and 5th steps, still elements far from the permanent magnet are also unnecessary subdivided (see Fig. 7(e)).

B. Simulation accuracy

Next, the accuracy of the obtained results is compared between the proposed and ZZ error estimation methods. Fig. 8 shows the transition of magnetic field energy error as the adaptive steps proceed in both, the proposed and ZZ methods.

The computation error using rough initial mesh was 32.6%. Using the proposed method, the error at 5th step finally decreases to 1.0% with 146,050 elements. The computation error of the ZZ method decreases to 8.6% at the 4th step, and remained unchanged to the 5th step, which leads to the main conclusion that the proposed method provides high-quality mesh with less number of elements and better accuracy, than that of the traditional ZZ method.

IV. Conclusion

In this paper, we have applied an error estimator based on the magnetic field conservation and a mesh improvement methodology using the non-conforming edge-based FEM to develop a new adaptive meshing method. The previously proposed error estimator based on the magnetic field conservation, in this paper, was extended and implemented to the adaptive meshing FEA. The proposed adaptive meshing generates better quality elements surrounding an object. As a result, the magnetic field error decreases from 32.6% to 1.0%, showing superiority to the traditional ZZ error estimation method.

In the future, authors intend to apply the proposed method to non-linear and magneto-dynamic problems utilizing hexahedral edge-based finite elements.

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